

Single-Cycle Instrument Deployment for Mars Rovers

L Pedersen¹, R. Sargent¹, M. Bualat, C. Kunz¹, S. Lee¹, A. Wright¹

NASA Ames Research Center, Moffett Field, CA 94035-1000, USA

¹QSS Group, Inc at NASA ARC

{lpedersen, rsargent, ckunz, sylee, awright}@arc.nasa.gov, Maria.G.Bualat@nasa.gov

Abstract

Future Mars rovers, such as the planned 2009 MSL rover, require sufficient autonomy to robustly approach rock targets and place an instrument in contact with them. It took the 1997 Sojourner Mars rover between 3 and 5 communications cycles to accomplish this on rocks. This paper describes the NASA Ames approach to robustly accomplishing single cycle instrument deployment, using the K9 prototype Mars rover. An off-board 3D site model is used to select science targets for the rover. K9 navigates to targets, using deduced reckoning, and autonomously assesses the target area to determine where to place an arm mounted microscopic camera.

Introduction

Approaching science targets, such as rocks, and placing instruments against them to take measurements is the most important function of a planetary surface exploration rover, such as the planned 2009 Mars Science Laboratory (MSL) rover (Figure 1). This is necessary to acquire samples, determine mineralogy, obtain microscopic images and other operations needed to understand the planet's geology and search for evidence of past or present life. Significant science simply cannot be done with remote measurements only.

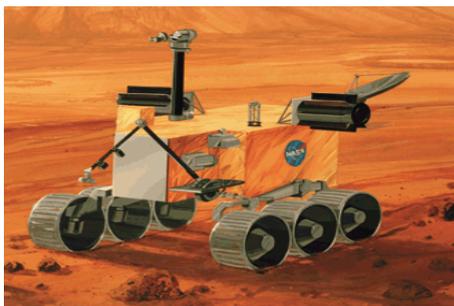


Figure 1 Artist's conception of 2009 Mars Science Laboratory (MSL) rover. Current plans call for a nuclear powered vehicle operating for up to 1000 days. [JPL]

Currently, a typical rover mission scenario starts when Mission Control uplinks a command sequence to the rover, specifying a detailed sequence of commands to take the rover to a particular target and deploy the desired instrument on it. The rover attempts to execute

it as best it can, stopping when either the goal has been achieved or, as is more likely, conditions are such that the original sequence is no longer applicable. This could be due to obstacles in the way, navigation errors leading to loss of the target, excessive power use or unforeseen complexity of the target that prevents the instrument from being placed anywhere against it. Rover status and sensor data are downlinked to mission control at the next communications opportunity. Mission Control then assesses the situation and decides on the next command sequence to uplink. Several such command, or communications, cycles may be needed to accomplish the objective.

The light speed time delay between Earth and Mars varies between 10 and 20 minutes depending on their relative locations. Depending on the communications assets in place, only one such command cycle may be possible per Martian day, or sol.

This operating paradigm works well for spacecraft. Although far from benign, the space environment is very predictable and command sequences for a week's worth of activities are feasible. It does not work well for rovers in the complex environment of a planetary surface, even a relatively static one such as Mars.



Figure 2 Sojourner rover, observed from the Pathfinder lander on Mars in 1997. [JPL]

The current *flight* state-of-the-art, the 1997 Sojourner Mars rover (Figure 2), requires at least 3 command cycles, each lasting a single sol, to accomplish the task of placing a relatively forgiving instrument on a compliant mounting against a rock several meters away. In addition, Sojourner could be observed by the Pathfinder lander, giving Mission Control a better view of the situation.

Reliability and verifiability are the fundamental concerns for flight missions and the reasons why

Sojourner had such limited autonomy. The rover could only execute rigid command sequences, the default response to unexpected behavior was to abort the sequence and wait for the next communications opportunity. The reasons for this is that these rigid sequences could be rigorously checked and verified by mission control prior to being uploaded to the vehicle, guaranteeing that a whole class of failure modes would not occur.

Long delays of multiple sols to investigate each science target are unacceptable for a comprehensive study of a planetary surface. The technology to accomplish this objective in a single command cycle is essential. The 2009 MSL rover, as currently envisioned, *cannot* accomplish its science objectives without such a capability [1].

The MSL rover will operate far away from the landing craft. It will carry more sophisticated instruments than Pathfinder, and these must be placed against rock targets, up to 10m distant, with significantly greater precision.

At NASA's Ames Research Center (ARC), we are developing the robust autonomous instrument deployment capability needed for Mars rover missions. Our rover, K9, has demonstrated fully autonomous deployment of a microscopic camera against a rock in a relatively complex outdoor test environment (Figure 3).



Figure 3 K9 rover approaches a rock target in the NASA Ames Marscape prior to autonomously placing the CHAMP microscopic camera against it using its 5 DOF robotic manipulator arm (August 2002).

This paper describes our overall system, the K9 robot plus associated hardware and software, and the demonstrated capabilities of our instrument placement system.

System Architecture and Technologies

A complex sequence of activities is required for a rover

to approach a target and place an instrument in contact with it (Figure 4). Currently, we primarily address the problem of instrument placement once the rover is at the target. However, for completeness, we begin with a review of methods for approaching the target.

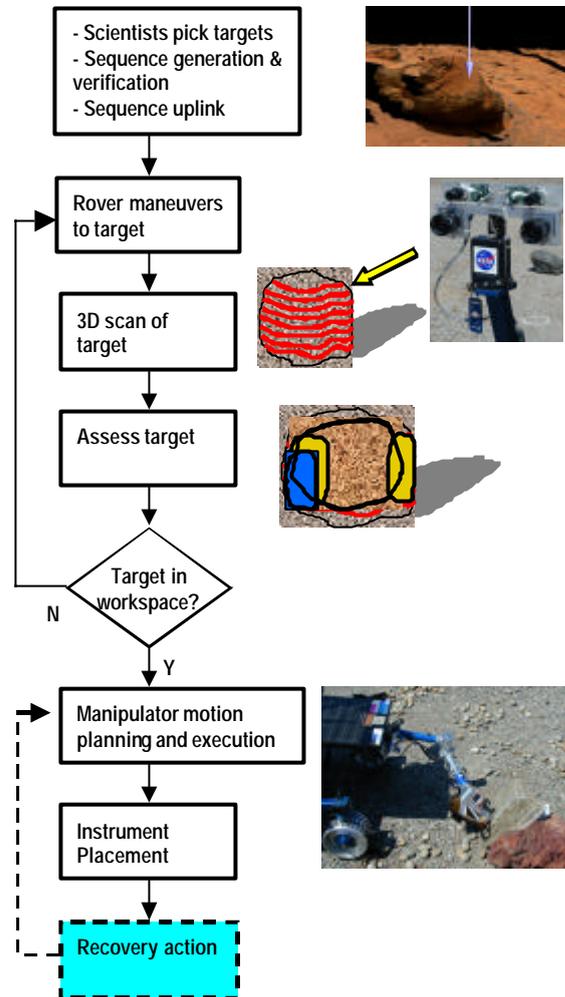


Figure 4 Simplified sequence of operation that must be performed by a rover, such as K9, to autonomously place instruments on a target.

Target Approach

First the rover must maneuver to within contact distance of the target. Because of navigation errors and uncertainty about the target location, the rover must keep track of the target location relative to itself throughout the maneuver. At the same time, it must avoid obstacles and pass through waypoints (if any).

Vision-based target tracking techniques can accomplish this. Visual tracking is a closed-loop system that measures error directly through sensory feedback. As the rover moves, images are acquired of the presumed target area. Target features, such as 2D texture or 3D shape, are compared to features derived from the images and used to update the relative position of the target with respect to the rover. Provided target "lock"

is maintained during the traverse, the target position relative to the rover can be obtained with relatively high accuracy. Initial uncertainties in target location, or those introduced by motion over unknown terrain, could potentially be eliminated by the visual tracking.

A 2D feature based visual servoing approach used on a previous rover at Ames, Marsokhod [2], relies on binary correlation to match features in the spatio-temporal image stream with features from a template image of the target. This is used to determine the target location in subsequent images acquired as the rover moves. Knowing the target location, a control loop keeps the rover navigation cameras foveated onto the target and directs the rover directly towards it.

Target Assessment and Instrument Placement

Once the rover has moved up to the target, it must determine where to place the instrument, what pose is needed, and check that the target surface will even permit the instrument to be placed there.

If Mission Control specified a particular final pose for the instrument, relative to a target that has been accurately tracked, then this task is unnecessary. The FIDO rover [4] demonstrated this. Using visual navigation techniques it can approach an exact target spot, localized from rover the with 3cm precision. Once there, FIDO lowers an arm-mounted microscopic camera from a point directly above the target until a focused image is acquired. However, taking measurements from above targets is not always sufficient. Arbitrary instrument poses may be needed.

Scientists at Mission Control might wish to specify an entire rock as a target, not just a given point. Not only is such over-specification unnecessary; it may over-constrain the problem, and might not even be feasible prior to the rover approaching close enough to the rock to see it in sufficient detail. Alternatively, it might simply not be possible to track a single point with enough precision. In these cases, scientists are compelled to request a measurement anywhere on a rock (or large area on it).

The first step in determining where to place an instrument anywhere on a rock target (or other large area) is to obtain a 3D scan of the work area. This can be done with stereo cameras. It is important that they be well calibrated with respect to the rover manipulator arm, as the derived 3D point cloud will be used to compute desired instrument poses.

Next, the rock (or target area) in the 3D model of the work area must be segmented from the background. We have developed an iterative 3D clustering algorithm [5], based on the statistical EM algorithm, for this purpose. This algorithm is very robust to noise, requiring only that the ground be relatively flat (but at

an arbitrary orientation) and the work area have at most one rock significantly larger than any clutter in the scene. If several large rocks are present in front of the rover, it becomes necessary for the workspace to be partitioned amongst them before applying this algorithm. Otherwise, it may aggregate several rocks together as a single rock or segment a random selection. Rocks piled up together will be aggregated.

The segmentation algorithm does not require many 3D points from the workspace to segment it. Therefore, the acquired 3D point cloud from the scene can be aggressively sub-sampled, enabling this algorithm to execute very rapidly.

Next, all points in the target area must be checked for consistency with the rover instrument to be placed. The simplest check for each point is to find all points within a given radius, compute the best-fit plane, and check the maximum deviations do not exceed some preset tolerance. The points are prioritized according to how flat the area is. Doing this also gets us the surface normal at each point in the target area. The result is a prioritized list of instrument positions and orientations .

Finally, the instrument can be placed. First, via a series of pre-planned waypoints the arm is un-stowed and put in a holding position. Next it goes to a pose near the highest priority target pose in the workspace, holding back a safe distance along the target surface normal. To compensate for possible small errors in surface location, the instrument's final approach is along the measured normal to the target rock face, moving slowly forward until contact is confirmed by mechanical sensors.

K9 Rover

The K9 rover (Figure 3) is mechanically identical to the FIDO rover, itself an advanced technology rover that is a terrestrial prototype of the rover that NASA/JPL plans to send to Mars in 2003 (see <http://fido.jpl.nasa.gov>). K9's mobility sub-system consists of a six-wheel rocker-bogie suspension system and is capable of traversing over obstacles up to 30 cm in height.

The main CPU is a 750 MHz PC104+ Pentium III running the Linux operating system. An auxiliary microprocessor communicates with the main CPU over a serial port and controls power switching and other I/O processing. The motion/navigation system consists of motor controllers for the wheels, arm joints, and pan/tilt unit, a compass/inclinometer, and an inertial measurement unit.

The K9 rover software architecture uses the Coupled Layered Architecture for Robotic Autonomy (CLARAty) [7] developed at JPL, in collaboration with ARC and Carnegie Mellon University. By developing our instrument placement technology under the CLARAty architecture, we can easily port the system to

other robots running CLARAty.

K9 Cameras

K9 is equipped with a front-mounted forward looking pair of b/w stereo hazard cameras and mast-mounted stereo pairs of high resolution color science cameras and wide field of view b/w navigation cameras (Figure 5). The navigation and science stereo camera pairs are mounted on a common pan-tilt unit, and can acquire image panoramas from around the rover.



Figure 5 K9 Stereo Hazard cameras, at the front of the rover, overlook the arm workspace (left) Navigation cameras and high-resolution science stereo camera pairs on a pan tilt unit are mounted on K9's mast(right).

The hazard cameras overlook the arm workspace. Being fixed, and close to the target area, they are the easiest to calibrate with respect to the arm, and are therefore the current means for 3D scanning of the target area.

The hazard cameras are calibrated using a custom target mounted to the arm's end-effector (Figure 6). The target is designed such that every 3x3 subset of the checkerboard can be uniquely identified, so that corresponding points may be matched between cameras even if the target is partly outside the view of one or both (Figure 7).

After taking several image pairs with different arm configurations and identifying the intersections in each image, we derive the camera intrinsic parameters, and an initial estimate of the extrinsic parameters using the OpenCV computer vision package. We then refine the extrinsic camera parameters, as well as the estimate of the location of the target with respect to the end-effector, by adjusting the parameters while minimizing the total projection error over all the image pairs taken. The resulting model is a full characterization of the relationship between the two cameras, and between the cameras and the arm, so that stereo depth images taken with the cameras can be immediately used for arm positioning.

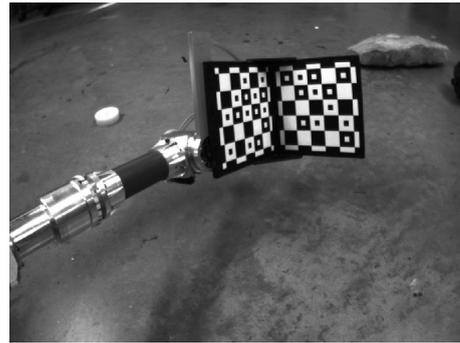


Figure 6 Hazard camera image of calibration target mounted on manipulator arm, used for the combined calibration hazard cameras and manipulator arm.

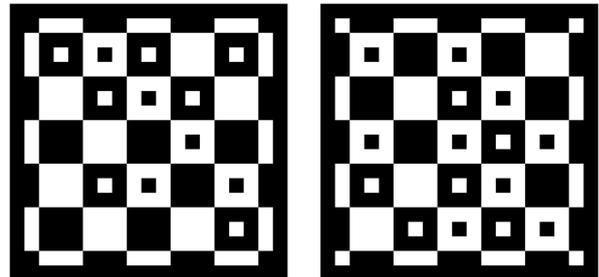


Figure 7 Each 3x3 subset of the target checkerboard is unique.

Manipulator Arm



Figure 8 K9 5 DOF manipulator arm, with CHAMP microscopic camera mounted at the end. Note the hazard cameras (top right) overlooking the arm workspace.

K9's instrument arm (Figure 8) is a 5-DOF robotic manipulator based on 4 DOF FIDO MicroArm IIA design from JPL [8]. It is approximately 5.0 kg with a total extended length of 0.79 meters. The waist yaw, shoulder pitch, elbow pitch, forearm twist (designed at Ames), and wrist pitch joints of the arm allow arbitrary x-y-z instrument placement as well as pitch and yaw control within the arm workspace. These rotational aluminum joints are connected by graphite epoxy tube links. The links are configured in a side-by-side orientation, with the two links running directly next to

each other.

CHAMP Microscopic Camera

Affixed at the end of K9's arm is the CHAMP (Camera Hand-lens MicroscopPe) microscopic camera [9] (Figure 8). It has a movable CCD image plane, allowing it to obtain focused images over a wide depth of field, from a few millimeters up to several meters.

Rotation about CHAMP's long axis does not need to be controlled, therefore the 5 degrees of freedom of K9's arm are sufficient to place CHAMP flat against a rock target. The rover's base only needs to move to within arm's reach of the rock and can remain stationary during arm movement.

CHAMP has three spring-loaded mechanical distance sensors around its face (Figure 13) that report contact with the rock. Because the rock surface is known to be flat, these three such sensors are sufficient for the final placement of the instrument.

CHAMP can acquire a Z-stack of images from a target, each focused at a slightly different depth. These can be combined into a composite focused image or 3D mesh through a two step process: first, each pixel in each image is assigned a focus value corresponding to the sum of absolute differences among pixels within a small window around the pixel. The images are then registered to each other (this step is necessary because of wind and vibration, especially at extremely close range), using the phase shift correlation algorithm described in [10][11]. Finally, the pixels that are most in-focus down a given column in the stack are selected for the composite image (Figure 14). Using focus motor position information, each in-focus pixel can be projected into 3-space, allowing for the reconstruction of a 3D mesh.

Instrument Placement Demonstration

K9 first successfully demonstrated autonomous instrument placement in 2002. Using odometry and deduced reckoning, K9 navigates to targets up to 3m distant (Figure 3).



Figure 9 Rock target scene in front of rover. Rock targets are not in dead center of manipulator workspace due to navigation inaccuracies.

The Ames Marscape outdoor test site has moderate clutter, including scattered cobble and loose soil. Some target rocks themselves are actually complex aggregates of many rocks, with a smooth surfaces and grossly misshapen (Figure 9). Note the different textures and colors.

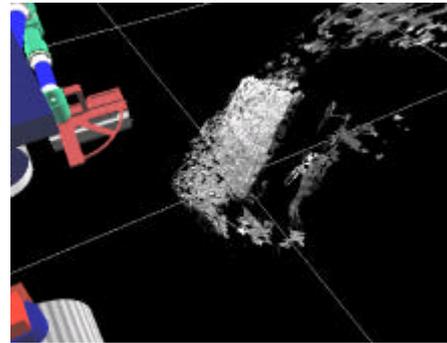


Figure 10 K9 3D model of rock targets as rendered in Viz.

Figure 10 shows the 3D model, constructed onboard K9, using stereo hazard camera images of the rock scene in Figure 9. This dot cloud model is passed on to the 3D rock/ground segmentation routine (Figure 11) to determine which part of the scene is the target rock. Points on the rock surface are checked to ensure that CHAMP can be safely placed there (Figure 12). A point is considered acceptable if all rock points within a 5 cm radius are within 1 cm of the best-fit plane. The good points are prioritized according to flatness and amount of usable stereo data.

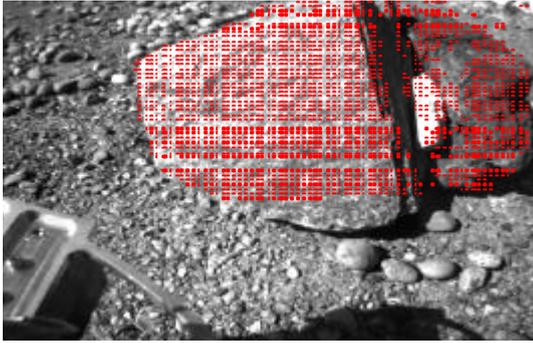


Figure 11 Rock points from above dot cloud superimposed on image of work area. All rock points within 5 cm of ground plane are excluded to ensure instrument safety. Blank areas within rock are caused by missing data in the dot cloud (due to inadequate texture for stereo correlation in those areas).

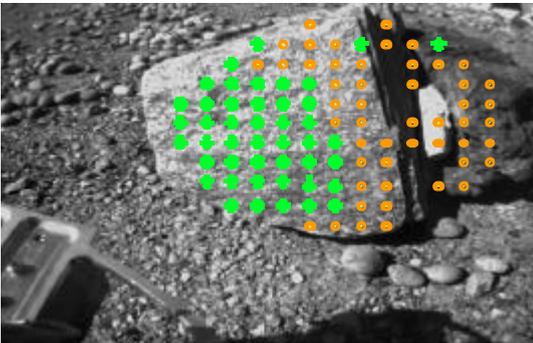


Figure 12 Locations on target rocks tested for consistency with the CHAMP microscopic camera. Large green points are considered safe for CHAMP.

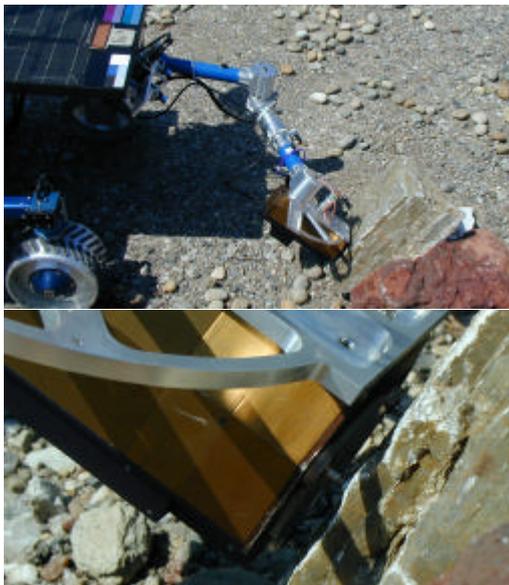


Figure 13 **Top:** Final placement of CHAMP against the rock at the highest priority reachable point. **Bottom:** Close-up view of CHAMP showing the contact sensors pushed up against the target rock surface.

CHAMP is placed on the highest priority point, in this case this was on the flat surface, within the rover workspace (Figure 13). Figure 14 show the focused composite image obtained from the Z-stack of images that CHAMP obtained *autonomously* of this rock scene.

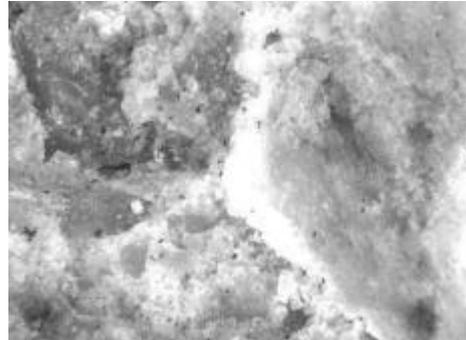


Figure 14 Focused composite of a Z-stack of CHAMP microscopic images obtained after final placement on the target rock. Image misalignments due to wind induced rover motion are automatically corrected. Maximum resolution is approximately 50 um per pixel, sufficient to show fine crystal structures.

Future Work

Our next step is to incorporate the visual servoing technology under development at both Ames and JPL [2][3][4]. This will enable K9 to autonomously keep track of a distant target as it approaches it, and brings it within the arm workspace.

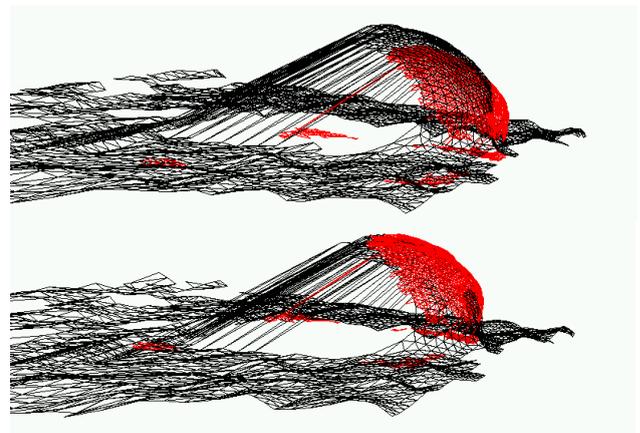


Figure 15 **Top:** Side-view of unaligned K9 hazcam and mast camera stereo models superimposed (hazcam in red). **Bottom:** Same two models after model registration.

While we track targets with steerable cameras on K9's mast, the target must be "handed off" to K9's fixed hazard cameras which have the best view of the workspace and are the best calibrated with respect to the arm. Mechanical repeatability of the pan-tilt head limits the accuracy with which we may determine the relative pose between the hazard cameras and mast

cameras. We are developing techniques to automatically align stereo models taken simultaneously from the hazcams and the mast cameras (Figure 15) [13]. By aligning hazcam and mast camera stereo models, the relative camera pose can be determined very accurately, allowing us to map target location from one camera set to the other.

Systematic end-to-end testing in realistic field environments is essential to make the system reliable enough. So far, modest reliability has been demonstrated in a relatively simple environment. Our final goal is a very robust system capable of operating in a complex Martian environment that includes many rocks and significant clutter (Figure 16). Towards this, we are integrating our system with a simulation facility [12] and are planning field tests in both the Ames Marscape test facility and an undisclosed desert location.

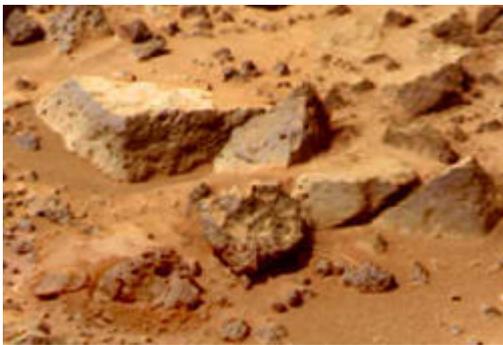


Figure 16 Mars rock scene, with significant clutter, few color variations and overlapping rocks of comparable sizes.

Conclusions

Autonomous instrument placement in one command cycle is the single most important capability for increasing the science return of future missions. It is essential for the 2009 MSL mission which, as currently planned, cannot accomplish its scientific objectives without it. This work demonstrates the eminent feasibility of autonomously, and robustly, placing science instruments against a rock target.

Acknowledgments

The authors of this paper would like to acknowledge the support of the Autonomy and Robotics Area managers, James Crawford and Nicola Muscettola, at the Computational Sciences Division at NASA Ames Research Center. We gratefully acknowledge the contributions of the following people: Judd Bowman, Howard Cannon, Larry Edwards, Michael Fair, David Lees, Eric Park, Aaron Rolett, Richard Washington, Hoang Vu, and the CHAMP instrument development team from LASP. We would also like to thank the

Intelligent Systems and the Mars Technology programs for their support.

References

- [1] Krasner, S.M., Tamppari, L., Steve Peters, S., Limonadi, D. (2002), "MSL Scenarios and Autonomy Requirements", MPSET meeting 4/11/2002.
- [2] Wettergreen, D., H. Thomas, M. Bualat, (1997) "Initial Results from Vision-based Control of the Marsokhod Rover," in *proc. IEEE/RSJ International Conference on Intelligent Robots and Systems*, Grenoble, France, September 7-12, 1997.
- [3] Nesnas, I., M. Maimone, H. Das (2000), "Rover Maneuvering for Autonomous Vision-Based Dexterous Manipulation", *proc. IEEE International Conference on Robotics and Automation*, San Francisco, CA, 2000.
- [4] Huntsberger, T., H. Aghazarian, Y. Cheng, E.T. Baumgartner, E. Tunstel, C. Leger, A. Trebi-Ollennu, and P.S. Schenker, (2002) "Rover Autonomy for Long Range Navigation and Science Data Acquisition on Planetary Surfaces", in *proc. IEEE International Conference on Robotics and Automation*, Washington, D.C. May 2002.
- [5] Pedersen, L., (2002) "Science Target Assessment for Mars Rover Instrument Deployment," in *proc. IEEE/RSJ International Conference on Intelligent Robots and Systems*, Lausanne, Switzerland, September 30 – October 4, 2002.
- [6] Bresina, J., K. Golden, D.E. Smith, R. Washington, (1999) "Increased Flexibility and Robustness for Mars Rovers", in *international Symposium on Artificial Intelligence, Robotics and Automation in Space*, 1999.
- [7] Nesnas, I., R. Volpe, T. Estlin, H. Das, R. Petras, D. Mutz, (2001) "Toward Developing Reusable Software Components for Robotic Applications," in *IEEE/RSJ International Conference on Intelligent Robots and Systems*, 2001.
- [8] Jet Propulsion Laboratory, "Planetary Dexterous Manipulators. MicroArm IIA and MastArm Specification Sheet."
- [9] Lawrence, G.M., J.E. Boynton, *et al*, (2000), "CHAMP: Camera HAndlens MicroscopE", in The 2nd MIDP Conference, Mars Instrument Development Program. JPL Technical Publication D-19508, 2000.
- [10] Kuglin C., and D. Hines, (1975) "The Phase Correlation Image Alignment Method", in *proc. IEEE International Conference on Cybernetics and Society*, pp163-165, 1975
- [11] Hill, L., (10 August 2001) <http://www.ee.surrey.ac.uk/Personal/L.Hill/pc.html>
- [12] L. Pedersen, M. Bualat, D. Smith, D. Lees, R. Washington (2003), "Integrated Demonstration of Instrument Placement, Robust Execution, and Contingent Planning" *To appear in proceedings of i-SAIRAS*, 2003.
- [13] M. Deans, C. Kunz, R. Sargent, L. Pedersen (2003), "Stereo Model Registration for Single-Cycle Instrument Placement," *To appear in proceedings of i-SAIRAS*, 2003
- [14] Flückiger, L. and C. Neukom, (2002), "A new simulation framework for autonomy in robotic missions," in *proc. IEEE/RSJ International Conference on Intelligent Robots and Systems*, Lausanne, Switzerland, September 30 – October 4, 2002.